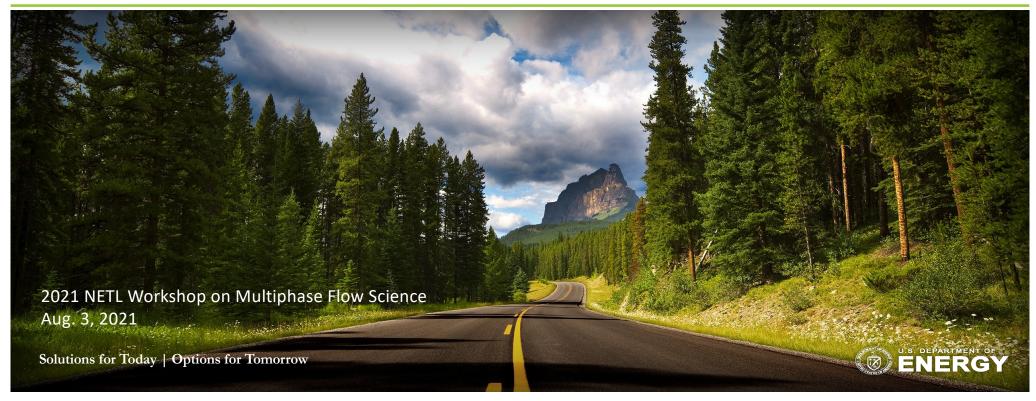
#### Calibration of a Particle-In-Cell Simulation Model for Gravitational Settling Bed Application



Aytekin Gel, Ph.D. Avinash Vaidheeswaran, Ph.D. Mary Ann Clarke, Ph.D.



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#### **Outline**



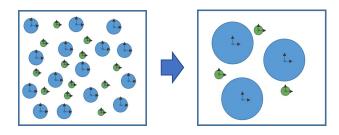
- Brief Overview of MFiX-PIC
- Representative Problems for the Calibration Study
- Brief Overview of Calibration Methods
- Simulation Campaigns to Construct Surrogate Models
- Assessment of Deterministic Calibration Results
- Concluding Remarks



#### **Brief Overview of MFiX-PIC**



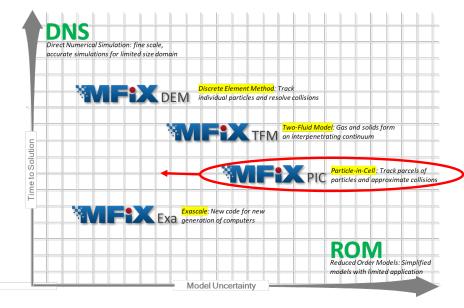
<u>Concept</u>: When particles are of equal physical property, they can be grouped together as larger parcels. Multiple particle types can be managed as separate parcel distributions.



Instead of managing each particle with Newtonian physics, parcel motion is influenced by a collisional stress model.

$$\frac{d\overrightarrow{V_p}}{dt} = \beta \left(\overrightarrow{U_g} - \overrightarrow{V_p}\right) - \frac{1}{\rho_p} \nabla p - \frac{1}{\epsilon_p \rho_p} \nabla \tau_p + \vec{g}$$

$$\tau_p = \frac{P_p \epsilon_p^{\gamma}}{\max \left(\epsilon_{cp} - \epsilon_p, \delta \left(1 - \epsilon_p\right)\right)}$$
Solids stress



A reduced computational load allows the simulations to proceed very rapidly. Lagrange tracking of parcels results in excellent visual graphics of statistically weighted particle motion.



#### Representative Problems for the Calibration Study



### Cases selected to cover a broad range of flow conditions

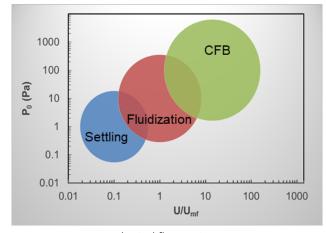
- Particle Settling:  $U/U_{mf} < 1.0 \ (P_0 \sim 1)$  (Simulation campaign)
- Bubbling Fluidized bed:  $U/U_{mf} \sim 1 (P_0 \sim 10)$
- Circulating Fluidized bed:  $U/U_{mf} >> 1.0 (P_0 \sim 100)$

## Parcel momentum equation $\frac{d\overrightarrow{V_p}}{dt} = \beta(\overrightarrow{U_g} - \overrightarrow{V_p}) - \frac{1}{\rho_p} \nabla p - \frac{1}{\varepsilon_p \rho_p} \nabla \tau_p + \overrightarrow{g}$ $\tau_p = \frac{P_0 \varepsilon_p^{\beta}}{\max \left(\varepsilon_{cp} - \varepsilon_p, \delta(1 - \varepsilon_p)\right)}$

#### Summary of model parameters used:

	t1 Pressure linear scale factor	t2 Volume fraction exponential scale factor	t3 Statistical weight	t4 Volume fraction at maximum packing	t5 Solid slip velocity factor	
C1: Particle Settling	[1,20]	[2,5]	[3,20]	[0.35,0.5]	[0.5,1.0]	
C2: Fluidization	[1,100]	[2,5]	[10,100]	[0.4,0.5]	[0.85,0.98]	
C3: Circulating Fluidized Bed	[1,250]	[2,5]	[4]	[0.4,0.5]	[0.85,0.98]	

<sup>\*</sup>Parameters selected based on prior sensitivity study



Hypothetical flow regime map



#### C1: Particle settling



#### **Problem setup**

Control variable: Initial solids concentration

Range: [0.05,0.25]

	x1: Initial solids concentration
C1: Particle Settling	[0.05,0.25]

Response variable: Location of filling shock (y2)

CFD results are compared with analytical solutions

# $\varepsilon_{s} = 0$ $\varepsilon_{s} = \varepsilon_{s0}$ $\varepsilon_{s} = \varepsilon_{s0}$ $\varepsilon_{s} = \varepsilon_{s0}$ $\varepsilon_{s} = \varepsilon_{s}$ $\varepsilon_{s} = \varepsilon_{s}$ t = 0 t > 0

#### Control variables: CFD (PIC parameters)

	t1 or (θ <sub>1</sub> ): Pressure linear scale factor	t2 or $(\theta_2)$ : Vol. fraction exponential scale factor	t3 or (θ₃): Statistical weight	t4 or (θ <sub>4</sub> ): Vol. fraction at maximum packing	t5 or (θ <sub>5</sub> ): Solid slip velocity factor
C1: Particle Settling	[0.48*, 20]	[2,5]	[2.96* , 20]	[0.35*, 0.5]	[0.5 , 1.0]

<sup>\*</sup> Initial targeted lower bound might be slightly different than actual samples generated as part of Latin Hypercube sampling

#### **Analytical Solution:**

Location of shock

$$x(t) = -t \left( \frac{\varepsilon_s^* \varepsilon_g^* u_r^* - \varepsilon_{s0} \varepsilon_{g0} u_{r0}}{\varepsilon_s^* - \varepsilon_{s0}} \right)$$

Rel. velocity (Stokes' drag)

$$u_r = \frac{g\Delta\rho d_p^2}{18\mu_g} \varepsilon_g^{3.65}$$

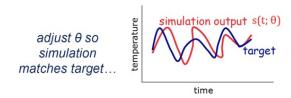


#### **Brief Overview of Calibration Methods**



#### **Deterministic versus Statistical Calibration**

 Maximize agreement between simulation and experiment target by improving the characterization of model parameters, θ<sub>i</sub> (e.g., P<sub>0</sub>, β) using available data.



- Also known as parameter estimation /identification, inverse problem modeling
- Calibration ≠ validation

Source: DAKOTA Software Training: Model Calibration (SAND2015-6813PE)

#### Two approaches:

- Deterministic Calibration:
  - Framed as minimization problem that seeks one or more sets of parameter values that reduce the error between simulation  $(s_i(\theta))$  and data  $y_i$ , typically in a norm:

$$\min_{\theta} f(\theta) = SSE(\mathbf{\theta}) = \sum_{i=1}^{n} [(s_i(\mathbf{\theta}) - y_i)]^2 = \sum_{i=1}^{n} [r_i(\mathbf{\theta})]^2$$

- Available in UQ software: DAKOTA (SNL), PSUADE (LLNL), OpenTURNS (Airbus+ONERA), Nodeworks (NETL) with some modifications
- Statistical calibration (Bayesian):
  - Instead of standalone parameter values, it seeks a statistical characterization of parameters most consistent with the data.
  - Available in UQ Software: PSUADE (LLNL), DAKOTA (SNL), OT, GPM/SA & SEPIA (LANL)





#### Calibration Proposed Settings for Model Parameters

- Utilize the constructed surrogate model and the set of analytical solutions (used in lieu of experiments) to perform the deterministic calibration.
- Deterministic calibration problem can be reframed as a minimization problem, i. e.,
- find a set of theta values that minimizes the residuals for all experiment data points Analytical solution  $\min_{\theta} f(\theta) = SSE(\theta) = \sum_{i=1}^{n} [(s_i(\theta) - y_i)]^2 = \sum_{i=1}^{n} [r_i(\theta)]^2$ Surrogate model evaluation for any

given  $\theta_1 \theta_5$  values

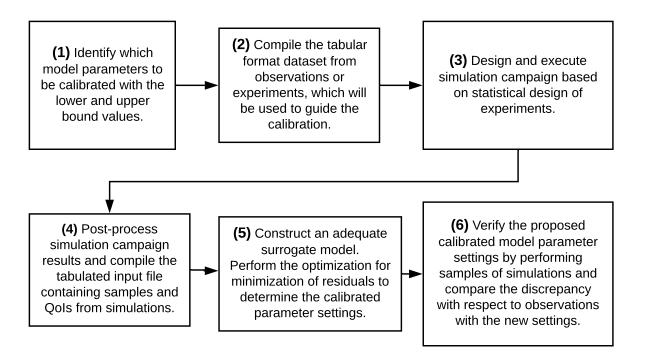
Utilized PSUADE and DAKOTA UQ toolkits to perform the optimization.

Recently implemented the workflow in Nodeworks



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#### Workflow



- Multiple step workflow followed for deterministic calibration procedure
- Design of the simulation campaign in Step (3) was carried out with Nodeworks, simulations were performed with MFiX-PIC on Joule 2.0
- Step (5) was performed with PSUADE, DAKOTA and Nodeworks by providing the same tabulated file that contains simulation campaign input and responses.

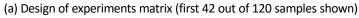


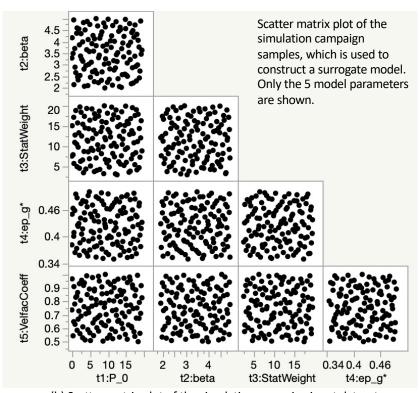
#### C1: Particle Settling Simulation Campaigns



#### Construct Surrogate Model from Simulation Campaign (120 samples)

	min	0.488	2.000	2.964	0.350	0.501	0.050
	max	20.000	5.000	20.008	0.500	1.000	0.250
		Uncertain	Input Parameters/Fa	ctors:			
Phases	MFIX-PIC	$\theta_1$	θ2	$\theta_3$	$\theta_4$	θ <sub>5</sub>	X1
as	Simulation	Emp.Pres.	Vol. Fraction Exp.	Stat.	Void Fraction	Solid slip	Initial solids
1	Number	Constant	Scale Factor	Weight	at max packing	velocity factor	concentratio
	1	4.375	2.965	4.388	0,478	0.707	0.243
	2	17.049	2.182	6.917	0.441	0.614	0.246
	3	3.860	2.817	8.729	0.368	0.761	0.128
	4	19.782	3.462	16,329	0,418	0.917	0.079
	5	1.572	2.662	18.853	0.495	0.830	0.098
	6	9.356	4.811	3.246	0.472	0.625	0.106
	7	4.613	3.656	19.361	0.363	0.990	0.173
	8	8.892	2.695	14.690	0.372	0.856	0.136
	9	15.462	4,566	19.936	0.407	0.818	0.075
	10	9.795	4.642	6.737	0.424	1.000	0.130
	11	14.360	3.700	18.536	0.489	0.636	0.089
	12	3.531	3.157	15.467	0.480	0.611	0.074
	13	18.016	3.374	5.465	0.373	0.541	0.157
	14	3.201	3.244	12.546	0.406	0.956	0.107
	15	11.773	2.120	16.688	0.470	0.732	0.132
	16	17.773	4.197	10.865	0.497	0.575	0.061
	17	12.139	3.181	17.799	0.350	0.803	0.154
	18	10.386	2.243	18.177	0.397	0.527	0.179
	19	6.361	4.267	8.992	0.395	0.640	0.137
	20	1.927	4.594	4.961	0.486	0.586	0.167
	21	7.923	3.308	17.454	0.433	0.579	0.095
	22	13.928	4.625	15.328	0.359	0.882	0.244
	23	2.432	4.554	13.349	0.429	0.728	0.239
	24	10.716	3.062	6.490	0.360	0.655	0.084
	25	15.648	2.557	6.035	0.490	0.771	0.110
	26	1.282	3.708	10.969	0.458	0.780	0.198
	27	3.034	4.347	18.420	0.474	0.691	0.183
	28	14.002	4.521	5.618	0.457	0.798	0.053
	29	6.734	2.274	3.743	0.435	0.878	0.102
	30	6.781	4.125	18.047	0.377	0.891	0.111
	31	14.277	2.025	7.665	0.376	0.850	0.190
	32	15.903	3.078	16.156	0.493	0.519	0.219
	33	17.346	2.876	19.556	0.459	0.921	0.126
	34	19.639	4.896	12.084	0.378	0.711	0.170
	35	18.600	4.322	4.181	0.444	0.751	0.152
	36	10.571	4.975	14.150	0.495	0.943	0.157
	37	12.609	2.867	3.183	0.431	0.576	0.174
	38	0.488	3.294	7.583	0.382	0.737	0.212
	39	5.184	3.023	14.355	0.390	0.717	0.058
	40	0.563	4.171	15.091	0.450	0.967	0.144
	41	2.085	2.477	15.783	0.426	0.866	0.205
	42	10.212	3.885	5.890	0.462	0.859	0.249





hown) (b) Scatter matrix plot of the simulation campaign input dataset
Optimal Latin Hypercube Sampling based Simulation Campaign



#### C1: Particle Settling Analytical Solution

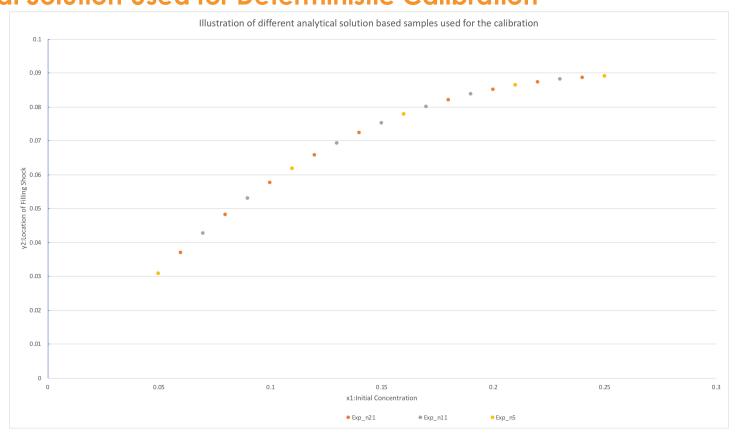


#### **Available Analytical Solution Used for Deterministic Calibration**

To guide the calibration process, analytical solution was used in lieu of actual experiments.

Three different scenarios are employed by computing the analytical solution for  $0.05 \le x1 \le 0.25$  range with different number of samples :

- 21 samples
- 11 samples
- 5 samples

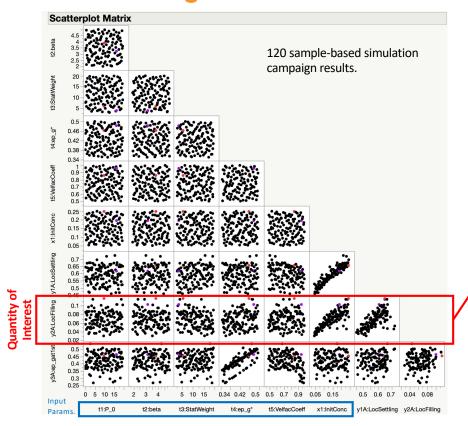


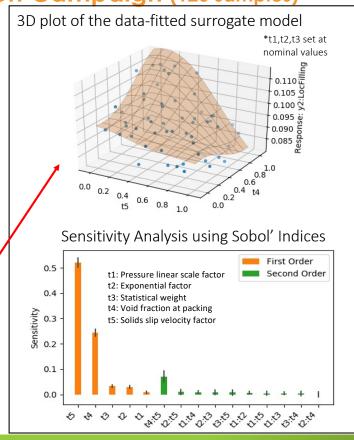


#### C1: Particle Settling Simulation Campaigns



Construct Surrogate Model from Simulation Campaign (120 samples)

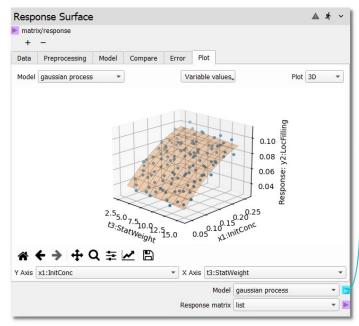








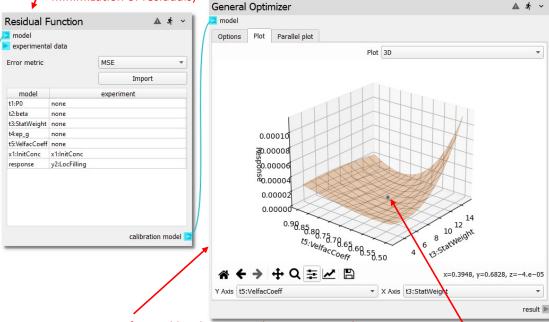
#### Illustration of Nodeworks Implementation Workflow



For more information on Nodeworks please visit: https://mfix.netl.doe.gov/products/nodeworks/ or please scan the QR code:



New node used to import experimental dataset and perform residual calculations required as part of the optimization (i.e., minimization of residuals)



Minimization performed by the General Optimizer node for:  $\min_{\theta} f(\theta) = SSE(\theta) = \sum_{i=1}^{n} [(s_i(\theta) - y_i)]^2 = \sum_{i=1}^{n} [r_i(\theta)]^2$ 

Optimal set of parameters identified that minimize the residual [9.55, 3.44, 9.41, 0.4, 0.69]

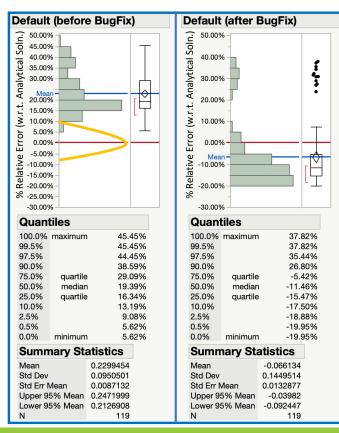


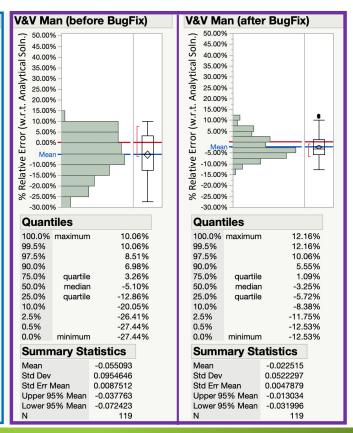
#### C1: Verification Simulation Campaigns (n=119)



#### Comparison of Histograms for % Rel. Error Before & After Bug Fix

MFIX-PIC model Parameter	Default Settings	V&V Manual Settings
(θ <sub>1</sub> ): Pressure linear scale factor	100	10
(θ <sub>2</sub> ): Vol. fraction exponential scale factor	3.0	3.0
Theta3 (03): Statistical weight	5.0	5.0
Theta4 (04): Vol. fraction at maxi- mum packing	0.42	0.4
Theta5 ( $\theta_5$ ): Solid slip velocity factor	1.0	0.5







#### C1: Proposed Calibrated Settings

Deterministic calibration with additional simulation campaigns

(using 120 samples with different bounds)



Simulation campaign with New Bounds [NB] (120 samples)

Bounds of the parameter space for Model Parameters

<b>Control variables: CFD</b> (PIC parameters)
--

C1: Particle Settling	t1 or $(\theta_1)$ : Pressure linear scale factor	t2 or $(\theta_2)$ : Vol. fraction exponential scale factor	t3 or (θ₃): Statistical weight	t4 or (θ <sub>4</sub> ): Vol. fraction at maximum packing	t5 or (θ <sub>5</sub> ): Solid slip velocity factor
Original Bounds [OB]	[0.48 , 20]	[2,5]	[2.96, 20]	[0.35 , 0.5]	[0.5 , 1.0]
New Bounds [NB]	[0.48, 20]	[2,5]	[2.94, 15]	[0.38, 0.43]	[0.5, 0.9]

Phases	MFIX.PIC Simulation Number 1 2 3 4 4 5 6 6 7 8 8 9 10 11 12 13 14 14 14 15 16 17 17 17 17 17 17 17 17 17 17 17 17 17	9 <sub>1</sub> Emp.Pres. Constant 4.375 17.049 3.860 19.782 1.572 9.356 4.613 8.892 15.462 9.795	put Parameters/F. 92  Vol. Fraction Exp. Scale Factor 2.965 2.182 2.817 3.462 2.662 4.811 3.656 2.695	θ <sub>3</sub> Stat. Weight 3.954 5.744 7.026 12.407 14.195 3.145	9 <sub>4</sub> Void Fraction at max packing 0.423 0.410 0.386 0.403 0.428	θ <sub>5</sub> Solid slip velocity factor 0.666 0.591 0.709 0.833	X1 Initial solids concentration 0.243 0.246 0.128
Phaset	Simulation Number  1 2 3 4 5 6 7 8 9 10 11 12 13	Emp.Pres. Constant 4.375 17.049 3.860 19.782 1.572 9.356 4.613 8.892 15.462 9.795	Vol. Fraction Exp. Scale Factor 2.965 2.182 2.817 3.462 2.662 4.811 3.656	Stat. Weight 3.954 5.744 7.026 12.407 14.195 3.145	Void Fraction at max packing 0.423 0.410 0.386 0.403	Solid slip velocity factor 0.666 0.591 0.709	Initial solids concentration 0.243 0.246
Pha	Number  1 2 3 4 5 6 7 8 9 10 11 12 13	Constant 4.375 17.049 3.860 19.782 1.572 9.356 4.613 8.892 15.462 9.795	Scale Factor 2.965 2.182 2.817 3.462 2.662 4.811 3.656	Weight 3.954 5.744 7.026 12.407 14.195 3.145	at max packing 0.423 0.410 0.386 0.403	velocity factor 0.666 0.591 0.709	0.243 0.246
	1 2 3 4 5 6 7 8 9 10 11 12 13	4.375 17.049 3.860 19.782 1.572 9.356 4.613 8.892 15.462 9.795	2.965 2.182 2.817 3.462 2.662 4.811 3.656	3.954 5.744 7.026 12.407 14.195 3.145	0.423 0.410 0.386 0.403	0.666 0.591 0.709	0.243 0.246
	2 3 4 5 6 7 8 9 10 11 12	17.049 3.860 19.782 1.572 9.356 4.613 8.892 15.462 9.795	2.182 2.817 3.462 2.662 4.811 3.656	5.744 7.026 12.407 14.195 3.145	0.410 0.386 0.403	0.591 0.709	0.246
	3 4 5 6 7 8 9 10 11 12	3.860 19.782 1.572 9.356 4.613 8.892 15.462 9.795	2.817 3.462 2.662 4.811 3.656	7.026 12.407 14.195 3.145	0.386 0.403	0.709	
	4 5 6 7 8 9 10 11 12	19.782 1.572 9.356 4.613 8.892 15.462 9.795	3.462 2.662 4.811 3.656	12.407 14.195 3.145	0.403		0.128
	5 6 7 8 9 10 11 12	1.572 9.356 4.613 8.892 15.462 9.795	2.662 4.811 3.656	14.195 3.145		0.833	
	6 7 8 9 10 11 12	9.356 4.613 8.892 15.462 9.795	4.811 3.656	3.145	0.428		0.079
	7 8 9 10 11 12	4.613 8.892 15.462 9.795	3.656			0.764	0.098
	8 9 10 11 12 13	8.892 15.462 9.795			0.421	0.600	0.106
	9 10 11 12 13	15.462 9.795	2.695	14.554	0.384	0.892	0.173
	10 11 12 13	9.795		11.247	0.387	0.785	0.136
-	11 12 13		4.566	14.961	0.399	0.755	0.075
	12 13	44.000	4.642	5.616	0.405	0.900	0.130
	13	14.360	3.700	13.970	0.426	0.609	0.089
		3.531	3.157	11.797	0.423	0.589	0.074
		18.016	3.374	4,716	0.388	0.532	0.157
		3.201	3,244	9,729	0.399	0.865	0.107
	15	11.773	2.120	12.662	0.420	0.685	0.132
	16	17,773	4.197	8.539	0.429	0.560	0.061
	17	12.139	3.181	13.448	0.380	0.742	0.154
H	18	10.386	2.243	13,716	0.396	0.522	0.179
	19	6.361	4.267	7.213	0.395	0.612	0.179
- 1	20	1.927		4.359		0.569	0.157
- 1			4.594	0.00	0.425		
- 1	21	7.923	3.308	13.204	0.408	0.563	0.095
- 1	22	13.928	4.625	11.699	0.383	0.806	0.244
- 1	23	2.432	4.554	10.297	0.406	0.683	0.239
- 1	24	10.716	3.062	5.442	0.383	0.624	0.084
L	25	15.648	2.557	5.120	0.427	0.716	0.110
L	26	1.282	3.708	8.613	0.416	0.724	0.198
- 1	27	3.034	4.347	13.888	0.421	0.653	0.183
	28	14.002	4.521	4.824	0.416	0.738	0.053
L	29	6.734	2.274	3.497	0.408	0.802	0.102
	30	6.781	4.125	13.624	0.389	0.813	0.111
	31	14.277	2.025	6.274	0.389	0.780	0.190
	32	15.903	3.078	12.285	0.428	0.515	0.219
	33	17.346	2.876	14.692	0.416	0.837	0.126
- [	34	19.639	4.896	9.402	0.389	0.669	0.170
- 1	35	18.600	4.322	3.807	0.411	0.701	0.152
ı	36	10.571	4.975	10.865	0.428	0.854	0.157
ı	37	12.609	2.867	3,100	0.407	0.561	0.174
1	38	0.488	3.294	6.216	0.391	0.689	0.212
- 1	39	5.184	3.023	11.010	0.393	0.673	0.058
	40	0.563	4.171	11.531	0.413	0.873	0.144
-	41	2.085	2.477	12.020	0.405	0.793	0.205
-	42	10.212	3.885	5,017	0.417	0.787	0.249
-	43	13.528	4.449	5.017	0.398	0.628	0.245
ŀ	44	7.214	5.000	5.892	0.381	0.721	0.148
- 1	44		5.000	5.692	0.381		
		0.994	4.944	13.008	0.397	0.619	0.082



#### C1: Proposed Calibrated Settings

MFIX-PIC model Parameters	Default Settings	V&V Manual Settings	PS Exp_n11 [NB]	DK Exp_n21 [NB]	PS Exp_n21 [NB]	DK Exp_n21 [OB]
Theta1 (01): Pressure linear scale factor	100	10	2.71	16.1	3.08	4.2
Theta2 ( $\theta_2$ ): Vol. fraction exponential scale factor	3.0	3.0	3.74	2.04	3.71	2.1
Theta3 (0 <sub>3</sub> ): Statistical weight	5.0	5.0	8.86	10.51	8.93	8.49
Theta4 (04): Vol. fraction at maxi-mum packing	0.42	0.4	0.4	0.4	0.4	0.38
Theta5 ( <b>0</b> <sub>5</sub> ): Solid slip velocity factor	1.0	0.5	0.7	0.53	0.69	0.66
Avg. % Rel. Err.	-6.61%	-2.25%	-5.9%	-2.63%	-6.17%	-2.53%
Min % Rel. Err.	-19.95%	-12.53%	-21.7%	-12.63%	-18.66%	-8.81%
Max % Rel. Err.	37.82%	12.16%	8.28%	7.09%	9.66%	5.23%



**Column Legend:** 

**Default Settings: Settings in MFiX-PIC** 

**V&V Manual Settings:** Settings determined by trial-error.

PS Exp\_n11 [NB]: Proposed calibrated model parameter settings obtained with PSUADE using a surrogate model constructed from the simulation campaign with new bounds and 11 samples of analytical solution to guide calibration

PS Exp\_n21 [NB]: Same as above except 21 samples of analytical solution employed.

**DK Exp\_n21 [NB]**: Proposed calibrated model parameter settings obtained with **DAKOTA** using a surrogate model constructed from the simulation campaign with **new** bounds and **11** samples of analytical solution to guide calibration

**DK Exp\_n21 [OB]**: Same as above except surrogate model constructed from the simulation campaign with original bounds used.

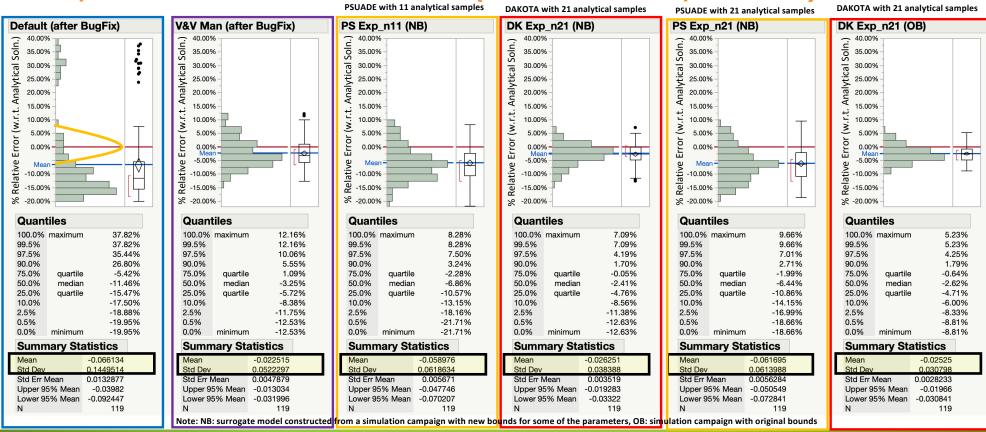
**Note:** % Rel. Err. Is the % Relative Error calculated by (Surrogate model evaluation – Analytical Soln.)/ Analytical Soln.



#### C1: Error Assessment of the Proposed Calibrated Settings



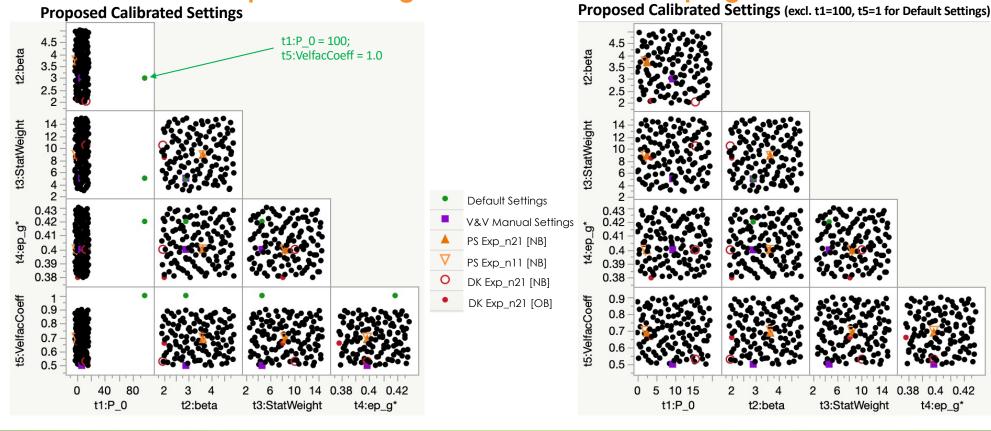
#### Comparison of PSUADE and DAKOTA (119 unseen samples for x1



#### C1: Proposed Calibration Settings



#### Visualization of Proposed Settings and Simulation Campaign





#### **Concluding Remarks**



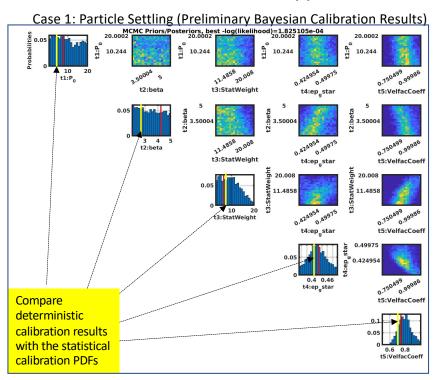
- MFiX-PIC offers substantial savings in time-to-solution, but the trade-off is accuracy.
- Objective was to employ various calibration techniques to assess the most uncertain model parameters specific to Parcel-in-Cell methodology and observe how they vary across different flow regimes.
- Adopted a systematic calibration procedure to identify optimal model parameter settings to minimize the discrepancy between MFiX-PIC and available experimental/analytical dataset. Started with Deterministic calibration as it is cheaper than Bayesian Calibration.
- Test the performance of calibrated model parameters rigorously. Also assessed the effect of varying sample size in the experiments (analytical solution).
- Explored different UQ toolkits such as PSUADE and DAKOTA and implemented the deterministic calibration capability within Nodeworks.
- When compared with the default settings, demonstrated significant accuracy improvement for Particle Settling case with deterministic calibration

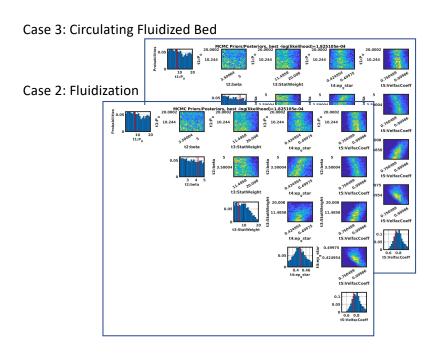


#### **Future Work**



 Perform deterministic calibration and statistical calibration for all selected cases and compare the outcomes from both calibration approaches







#### **Future Work**



• Compare proposed calibrated model parameter settings for different flow regimes and provide best practices guidance to MFiX-PIC users on how to set PIC specific parameters based targeted application. For example, for  $\theta_3$ :

Cases / Flow Regimes	t1 or (θ1): Pressure linear scale factor	t2 or $(\theta_2)$ : Vol. fraction exponential scale factor	t3 or (θ₃): Statistical weight	t4 or (θ₄): Vol. fraction at maximum packing	t5 or (θ₅): Solid slip velocity factor
C1: Particle Settling			10 10 10 10 10 10 10 10 10 10 10 10 10 1		
C2: Fluidization			300 5 10 15 20		
C3: Circulating Fluidized Bed			35 35 35 35 35 35 35 35 35 35 35 35 35 3		



#### References





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Note: QR codes for the URL of the references have been included to facilitate easy access via mobile devices.



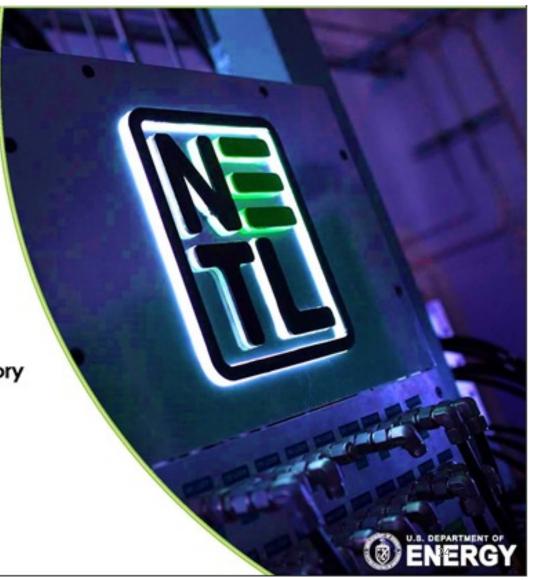
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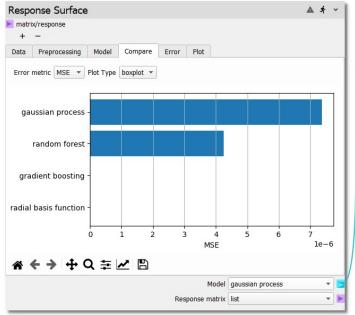


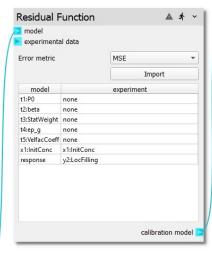


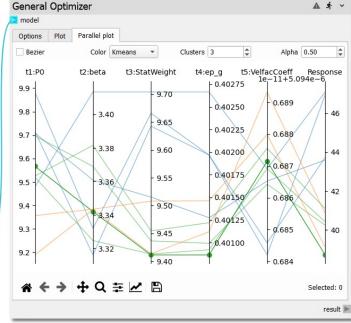
#### **Additional Slides**





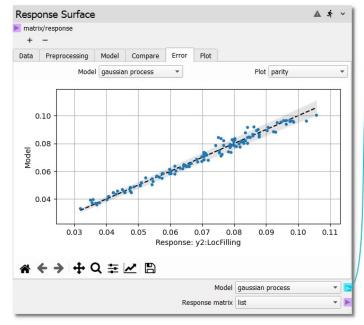




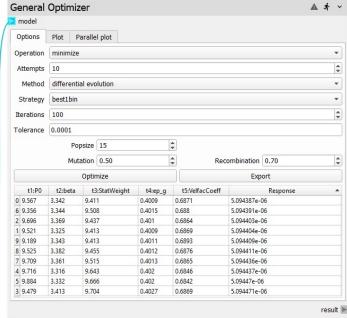






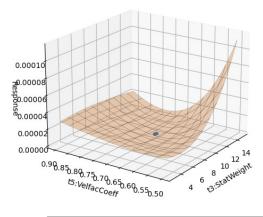


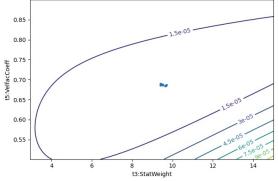


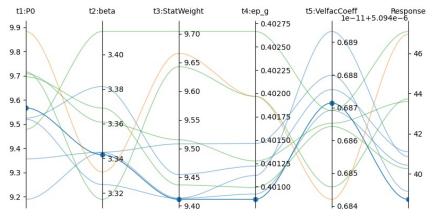














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